# International Journal of Innovative Research in Technology \& Science (IIIRTS) Field Functions with Surface-Defined Influential Radii and Their Applications 

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#### Abstract

In soft object modeling, soft objects are defined as a level surface of field functions, and a complex object can be connected smoothly through Boolean set blends. Because field functions are required to decrease to zero within the influential radius, union of soft objects is obtained easily by performing sum operation only, called soft blend. Besides, field functions with adjustable influential radii were also developed to adjust the size of the resulting set blends. However, the level surfaces of existing field functions always have similar shapes and sizes like the shape and size of soft object. As a result, unwanted blends and unnecessary bulges could be generated. To solve these problems, this paper proposes field functions with surface-defined influential radii, that is, it allow freely choosing implicit surfaces to define its inner and outer influential radii with any shapes. Thus, unwanted blend is removed by assigning blended primitives influential radii which does not contain the regions where unwanted blends lie; unnecessary bulge is avoided by assigning blended primitives influential radii which do not contain the region where unwanted bulges are located.


## 1. Introduction

In soft object modeling, primitive soft objects are defined as a 0.5 level-surface of field functions [1, 2, 3]. In order to create a more complex object, primitive soft objects, such as planes, super-ellipsoids, sweep surfaces, cylinders etc., can be connected smoothly through an automatically generated added or subtracted transition surface by Boolean set blends (union, intersection and difference). In the literature, boolean set blends include super-elliptical blends [4], blends with blending range parameters [5, 6] and blends of high-order smoothness [7]. Besides, sequential blends, i.e. a blend in blend, with affine-transformation are allowed and represented by a CSG (Constructive solid geometry) tree [8].

A field function is defined by a composition of a potential function and a distance function. Distance function [3, 9-14] determines the shape of a soft object. Potential function [1, 2, 11] enables the value of field function to decrease to zero in the influential radius and is zero outside the influential radius, and hence union of soft objects can be obtained by performing sum operation only, called soft blend [3] or by
product operations only, called Perlin's boolean set blends [15]. To offer these two families of blends more shape controls, some filed functions were also developed. Field functions in [1] offer a softness parameter to adjust a transition's curvature; field functions [16, 17] offer blend range control by offering an inner and an outer radius parameters to adjust the inner and the outer influential radii of a field function through a transform of distance function. Locally restricted blends [16] allows each primitive to locally have different influential radii, like blend range, with the others by using a deformation function of field function and a graph of influential weights on one another.

In fact, field function in [16] adjusts all the inner or the outer radii in all directions with the same parameter value, so the shapes of level surfaces of a field function are all similar. On the contrary, this paper develops field functions with surface-defined influential radii, which extends field function with adjustable influential radii [16] by adding a freely chosen modulation surface in any shape. By using every influential radius of the modulation surface to individually vary the outer radius or the inner radius parameter in every direction, the shapes of the level surfaces of the proposed field function in added-material blend region or in subtract-ed-material blend region vary gradually from the primitive's shape to the chosen modulation surface. Thus, if soft objects are defined using the proposed field functions, soft blend and Perlin's and Ricci's set blends have the following applications by choosing suitable modulation surface:

- Application 1: When one primitive generates two blends at different places with other primitives, one can remove one blend but keep the other unchanged by choosing a modulation surface to obtain a new added-material blend region without including the region where the unwanted blend lies.
- Application 2: Bulges are eliminated in a union of intersecting and connecting super-elliptic cylinders and supertoroids by choosing modulation surfaces such that their added-material blend regions do not overlap where the unwanted bulge lies, even though these blends do not have range parameters to do bulge elimination by gradi-ent-based methods [6, 18,19].


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The remainder of this paper is organized as follows: Section 2 reviews implicit surfaces. Section 3 reviews soft object modeling and existing field functions. Section 4 presents field functions with surface-defined influential radii to solve the problems stated in Section 3. Section 5 demonstrates the applications of the proposed field functions. Conclusion is given in Section 6

## 2. Implicit surface modeling

### 2.1. Primitive implicit surface

In implicit surface modeling, an primitive implicit surface is represented as a level surface of a defining function $f_{i}(x, y, z): R^{3} \rightarrow R$ by :

$$
\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z)=C\right\}
$$

where $C$ is set a constant $0,0.5$ or 1 . However, if the surface is viewed as an solid, it is redefined by a half space:

$$
\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z) \leq C\right\} \text { or }\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z) \geq C\right\}
$$

In the literature, according to the value of $C$, implicit surface modeling techniques have three categories:

- Zero implicit surface [19, 20, 21]:

$$
\begin{gathered}
\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z) \leq 0\right\},\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z) \geq 0\right\} \text { or } \\
\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z)=0\right\},
\end{gathered}
$$

whose compliment is $\left\{(x, y, z) \in R^{3} \mid-f_{i}(x, y, z) \leq 0\right\}$ or $\left.-f_{i}(x, y, z) \geq 0\right\}$

- Constructive geometry $[4,6]$ :

$$
\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z) \leq 1\right\} \text { or }\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z)=1\right\},
$$

whose compliment is $\left\{(x, y, z) \in R^{3} \mid 1 / f_{i}(x, y, z) \leq 1\right\}$.

- Soft object modeling [2, 5, 6, 6, 15, 18, 22]:
$\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z) \geq 0.5\right\}$ or $\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z)=0.5\right\}$.
whose compliment is $\left\{(x, y, z) \in R^{3} \mid 1-f_{i}(x, y, z) \geq 0.5\right\}$.
In the following, a surface is denoted by $f_{i}(x, y, z)=C$, and a soft object by $f_{i}(x, y, z)=0.5$


### 2.2. Implicit blends

Furthermore, based on a blending operator $B_{k}\left(x_{1}, \ldots, x_{k}\right)$ : $R^{k} \rightarrow R$, a more complex implicit surface is constructed from $k$ primitive implicit surfaces $f_{i}(x, y, z)=C, i=1, \ldots, k$, and is defined using a blend $B_{k}\left(f_{1}, \ldots, f_{k}\right)$ by

$$
\begin{gathered}
B_{k}\left(f_{1}(x, y, z), \ldots, f_{k}(x, y, z)\right)=C \text { or } \\
\left\{(x, y, z) \in R^{3} \mid B_{k}\left(f_{1}(x, y, z), \ldots, f_{k}(x, y, z)\right) \leq \text { or } \geq C\right\},
\end{gathered}
$$

where $B_{k}\left(f_{1}, \ldots, f_{k}\right)=C$ is called a blending surface. A blend connects primitive implicit surfaces smoothly by automatically generated added or subtracted transition surface which is tangent to blended primitives for eliminating sharp edges. Functionally, $B_{k}\left(f_{1}, \ldots, f_{k}\right)=C$ has three kinds denoted as fol-
lows: (a). Union: $B_{U k}\left(f_{1}, \ldots, f_{k}\right)=C$, (b). Intersection: $B_{l k}\left(f_{1}, \ldots, f_{k}\right)=C$, and (c). Difference of $f_{1}$ from $f_{2}, \ldots$, and $f_{k}$ : $B_{D k}\left(f_{1}, f_{2}, \ldots, f_{k}\right)=C$ as shown in Figure 1 , which defines a wheel by sequential blends, depicted as a CSG tree.


Figure 1. Wheel defined by $f(x, y, z)=B_{D 2}\left(B_{U 2}\left(B_{U 2}\left(f_{1}, f_{2}\right), f_{3}\right), f_{4}\right)=C$ and depicted as a CSG tree.

## 3. Soft object modeling

### 3.1. Definition of soft objects and their blends

A primitive soft object is defined using a field function as a defining function by

$$
\begin{equation*}
f_{i}(x, y, z)=(P \circ d)(x, y, z)=P(d(x, y, z))=0.5 \tag{1}
\end{equation*}
$$

where $d(x, y, z): R^{3} \rightarrow R_{+}$is called distance function and $P(d): R_{+} \rightarrow[0,1]$ is called potential function.

### 3.1.1. Distance function

A distance function $d(x, y, z)$ can be one of the structures: a point skeleton or 1D-3D skeletons [13]. As shown in Fig. 2, it is defined by

$$
r / I_{d}=\|\overrightarrow{o p}\| /\|\overrightarrow{o v}\|
$$

where $r=\left(x^{2}+y^{2}+z^{2}\right)^{0.5}$ is the short distance from $p(x, y, z)$ to the skeleton and $I_{d}$ is the influential radius specifying that the value of $(P \circ d)(x, y, z)$ is zero if $r \geq I_{d} . I_{d}$ can be viewed as the distance from the point $\boldsymbol{o}$ on the skeleton where $r$ is calculated to the surface $d(x, y, z)=1$ along the direction from $o$ to $p$. In fact, a ray-linear $f(x, y, z)$ can be used as a distance function $d(x, y, z)$ because it can be reformulated as $r / I_{f}$. Existing distance functions include parallel planes, one-branch

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plane [14], super-ellipsoids [3, 11], super-quadrics [23], generalized distance functions [10], skeletal primitives [12], sweep objects [13] and spherical product functions [14].

### 3.1.2. Potential function

Potential function $P(d)$ is required to decreasing from 1 to 0 as $d$ increases from 0 to 1 and satisfies the requirements $P(0)=1, P(0.5)=0.5, P^{\prime}(0)=0, P^{\prime}(1)=0$ and $P(d)=0$ for $d \geq 1$, all of which can be seen in Blanc's function $p=P_{b}(d)$ [1] written below:

$$
P_{b}(d)=\left\{\begin{array}{cc}
1-\left(3 d^{2}\right)^{2} /\left(s+(4.5-4 s) d^{2}\right) & d \leq 0.5  \tag{2}\\
\left(1-d^{2}\right)^{2} /\left(0.75-s+(1.5+4 s) d^{2}\right) & 0.5<d \leq 1 \\
0 & d>1
\end{array}\right.
$$

where $s$ is softness parameter.
The purposes of the requirements above are explained as below:

- $P(0.5)=0.5$ ensures that the shape of $P(d(x, y, z))=0.5$ is the same as $d(x, y, z)=0.5$ as in Figure 2. This tells that distance function determines the shape of a soft object.
- $P(0)=1, P(0.5)=0.5$ and $P(d)=0$ for $d \geq 1$ ensures that the value of $P(d(x, y, z))$ drops gradully to zero and is always zero when the value of $r$ exceeds the influential radius $I_{d}$.
- Decreasing $P(d), P^{\prime}(0)=0$ and $P^{\prime}(1)=0$.


Figure. 2. Influential radius $I_{r}=\|\overrightarrow{o l}\|$ of a distance function $d(x, y, z)$, an ellipsoid, in $x-y$ plane.

Because of these requirements, primitive soft objects $P(d(x, y, z))=0.5, i=1, \ldots, k$, can be blended easily by sum and product operations only such as the blends below:
(a). Soft blend [2, 11]:

Union: $\quad B_{S U k}\left(f_{1}, \ldots, f_{k}\right)=f_{1}(x, y, z)+\ldots+f_{k}(x, y, z)=0.5$.
(b). Perlin' set blends [15]:

Union: $\quad B_{P U k}\left(f_{1}, \ldots, f_{k}\right)=1-\left(1-f_{1}\right)^{*}\left(1-f_{2}\right) *\left(1-f_{k}\right)=0.5$;

Intersection: $\quad B_{P l k}\left(f_{1}, \ldots, f_{k}\right)=f_{1} * f_{2} * \ldots * f_{k}=0.5$;
Difference: $\quad B_{P U k}\left(f_{1}, f_{2} \ldots, f_{k}\right)=f_{1 *}\left(1-f_{2}\right)^{*} \ldots *\left(1-f_{k}\right)=0.5$.
In addition, some other blends with special functions on soft objects are listed below:
(a). Super-ellipsoidal blends [21], such as:

Union: $\quad B_{R U k}\left(f_{1}, \ldots, f_{k}\right)=\left(f_{1}{ }^{n}+\ldots+f_{k}^{n}\right)^{1 / n}=0.5$.
Intersection: $B_{R l k}\left(f_{1}, \ldots, f_{k}\right)=\left(f_{1}^{-n}+\ldots+f_{k}^{-n}\right)^{-1 / n}=0.5$.
where $n$ is a curvature paremeter to adjust the curvature of the transition surface.
(b). Blends with blending range parameters [4, 15], which allow to adjust the size of the transition of a blend by varying the values of range parameters. These blends combined with gradient-based variable blending range [12, 15] can also eliminate unnecessary bulges. Figure 3 shows sequential unions of six intersecting cylinders by $B_{U 2}\left(B_{U 2}\left(B_{U 2}\left(B_{U 2}\right.\right.\right.$ $\left.\left.\left.\left.\left.\left(B_{U 2}\left(f_{1}, f_{2}\right), f_{3}\right), f_{4}\right) f_{5}\right), f_{6}\right)\right)\right)=0.5$ without and with bulge eliminations, respectively.


Figure 3. Sequential unions of six end-to-end connecting and intersecting cylinders defined with and without bulges.

### 3.2. Field functions with adjustable inner and outer influential radii

As shown in Figure 2, influential radius $I_{d}$ can be divided into inner radius $\overrightarrow{o s}=I_{d} / 2$ and outer radius $\overrightarrow{s i}=I_{d} / 2$ and the inner radius and the outer radius influence the sizes of the subtracted-material (intersection) and the added-material (union) blending regions, respectively. The length of inner and outer radii indicate that a large soft object has a large blending region, a small one a small blending region.

To enable the adjustment of the lengths of inner and outer influential radii, field functions with adjustable inner and outer influential radii were proposed in $[6,17]$ and one of them is introduced as follows:

$$
\begin{equation*}
f_{i}(x, y, z)=\left(P \circ T_{*} \circ d_{i}\right)(x, y, z), \tag{9}
\end{equation*}
$$

where $T *(d)$ is a transform of $d_{i}(x, y, z)$, mapping [0.5(1-w $w_{2}$,

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$0.5]$ to $[0,0.5]$ or $\left[0.5,0.5\left(1+w_{1}\right)\right]$ to [0.5, 1]. For example, $T *(d)$ can be the normalization and affine transform $T_{n}(d)$ [6] given by

$$
T_{n}(d)=\left\{\begin{array}{cc}
1 & d>0.5\left(1+w_{1}\right)  \tag{10}\\
(d-0.5) / w_{1}+0.5 & 0.5 \leq d \leq 0.5\left(1+w_{1}\right) \\
N_{n}(d)=A d^{2}+B d+C & 0.5\left(1-w_{2}\right) \leq d<0.5 \\
0 & \text { otherwise }
\end{array}\right.
$$

and $w_{2} \leq 2 w_{1}, w_{2} \leq 1$ and $w_{1}>0 ; A=2\left(1 / w_{1}-1 / w_{2}\right) / w_{2}, B=1 / w_{1}-A$, $C=0.5-0.5 B-0.25 A$.

Thus, if soft objects are defined by $\left(P \circ T_{n} \circ d_{i}\right)(x, y, z)=0.5$, then adjusting $w_{2}$ and $w_{1}$ enables the inner and the outer radii change from $\overrightarrow{o s}=I_{d} / 2$ and $\overrightarrow{s t}=I_{d} / 2$ to $\overrightarrow{u s}=w_{2} I_{d} / 2$ and $\overrightarrow{s t}=w_{1} I_{d} / 2$, respectively and so subtracted-material and add-ed-material blending regions become located in 0.5(1$\left.w_{2}\right) \leq d_{i}(x, y, z) \leq 0.5$ and $0.5 \leq d_{i}(x, y, z) \leq 0.5\left(1+w_{1}\right), i=1, \ldots, k$, respectively, as shown in Figure 4.


Figure 4. Inner radius $\overrightarrow{u s}=w_{2} I_{d} / 2$ and outer radius $\overrightarrow{s t}=w_{1} I_{d} / 2$ of $(P \circ T * \circ d)=0.5$ of a ellipsoid in $x-y$ plane and its subtract-ed-material and added-material blending regions bounded by new ellipsoids in red and blue lines.

### 3.3. Shapes of the level surfaces of existing field functions

When soft objects are defined by $\left(P \circ T_{*} \circ d_{i}\right)(x, y, z)=0.5$, $i=1, \ldots, k$, in Eq. (9), in soft blend or Ricci's or Perlin's set blends $B_{k}\left(f_{1}, \ldots, f_{k}\right)=0.5$ in Eqs. (3)-(8) level surfaces $d_{i}(x, y, z)=l, 0.5\left(1-w_{2}\right) \leq l \leq 0.5\left(1+w_{i}\right)$, are used to generate the transition. Because $d_{i}(x, y, z)$ is always ray-linear, level surfaces $d_{i}(x, y, z)=l$ enlarge proportionally in all directions and have similar shapes as $l$ increases. To enable level surfaces $d_{i}(x, y, z)=l$ of $\left(P \circ T_{*} \circ d_{i}\right), 0.5\left(1-w_{i 2}\right) \leq l \leq 0.5\left(1+w_{i 1}\right)$, to have shapes different from soft object $d_{i}(x, y, z)=0.5$, this paper proposes field functions with surface-defined influential
radii, denoted by $\left(P \circ T_{a^{*}} \circ d_{i}\right)$ and $\left(P \circ T_{s^{*}} \circ d_{i}\right)$, which is extended from $\left(P \circ T * \circ d_{i}\right)(x, y, z)$ in Eq. (9) by adding a freely chosen modulation surface $f_{a i}(x, y, z)=0.5$ or $f_{s i}(x, y, z)$ $=0.5$ in shapes different from the primitives. Thus, as shown in Figure 5, by means of modulating the inner or the outer influential radius parameter $w_{1}$ and $w_{2}$ of $T *$ for every point's calculation through the influential radii $0.5 I_{s i}$ and $0.5 I_{a i}$ bounded by $f_{a i}(x, y, z)=0.5$ or $f_{s i}(x, y, z)=0.5$ in every direction:
(1). The shapes of $\left(P \circ T_{a^{*}} \circ d_{i}\right)(x, y, z)=l$ for $l=0.5$ to 0 , enlarge gradually from $d_{i}(x, y, z)=0.5$ to $f_{a i}(x, y, z)=0.5$ and its added-material blend region becomes $\left\{(x, y, z) \in R^{3} \mid d_{i}(x, y, z)\right.$ $\geq 0.5$ and $\left.f_{a i}(x, y, z) \leq 0.5\right\}$.
(2). The shapes of $\left(P \circ T_{s^{*}} \circ d_{i}\right)(x, y, z)=l$ for $l=0.5$ to 1 shrink gradually from $d_{i}(x, y, z)=0.5$ to $f_{s i}(x, y, z)=0.5$ and its subtract-ed-material blend region becomes $\left\{(x, y, z) \in R^{3} \mid f_{s i}(x, y, z) \geq 0.5\right.$ and $\left.d_{i}(x, y, z) \leq 0.5\right\}$.


Figure 5. Inner radius $\overrightarrow{o s}=I_{d} / 2$ and outer radius $\overrightarrow{s l}=w_{1} I_{d} / 2$ of $\left(P_{b} \circ T_{n} \circ d\right)=0.5, w_{1}=w_{2}=1$, of a ellipsoid in $x-y$ plane become $\overrightarrow{u s}=0.5\left(I_{d}-I_{s i}\right)$ and $\overrightarrow{s t}=0.5 I_{a i}$ by varying $w_{1}$ and $w_{2}$ of $T_{n}$ via chosen modulation surfaces sphere $f_{s}(x, y, z)=0.5$ and superellipsoid $f_{a}(x, y, z)=0.5$ in red and blue lines. The addedmaterial blending region of $\left.P \circ T_{a n} \circ d\right)=0.5$ become bounded by $d(x, y, z)=0.5$ and $f_{a}(x, y, z)=0.5$. The subtracted-material blending region of $\left(P \circ T_{s n} \circ d\right)=0.5$ become bounded by $f_{s}(x, y, z)=0.5$ and $d(x, y, z)=0.5$.

Thus, due to the shape change of the level surfaces in the blending region controlled by modulation surfaces, soft blend and Perlin's and Ricci's set blends on soft object ( $P$ 。 $\left.T_{s^{*}} \circ d_{i}\right)(x, y, z)=0.5$ have the following new functions by choosing suitable modulation surfaces $f_{a i}(x, y, z)=0.5$ or $f_{s i}(x, y, z)=0.5$ :

- Application 1: When one primitive has two blends with


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other primitives at two places, one can avoid one blend unwanted but keep the other unchanged by choosing a modulation surface to define a new added-material blend region without containing the region where the unwanted blend lies.

- Application 2: Bulge elimination for a union of intersecting and connecting super-elliptic cylinders and supertoroids is achieved by choosing modulation surfaces such that their union blend regions do not overlap where the unwanted bulge lies.


## 4. Field functions with surfacedefined influential radii

Let $T *(d)$ denotes a transform of distance function $d_{i}(x, y, z)$ like $T_{n}$ in Eq. (9). Extended from $\left(P \circ T_{*} \circ d_{i}\right)(x, y, z)$, field functions with surface-defined influential radii, denoted by $\left(P \circ T_{s^{*}} \circ d_{i}\right)(x, y, z)$, for union, intersection and difference are presented in Sections 4.1-3.

### 4.1. Field functions with surface-defined outer radius for a union blend $B_{u k}\left(f_{1}, \ldots, f_{k}\right)=0.5$

For each primitive $f_{i}$ in $B_{U k}$, define a field function as described below:
Step 1: Choose a surface $f_{a i}(x, y, z)=0.5$ that satisfy the conditions: (a). $f_{a i}(x, y, z)$ is ray-linear, (b). it and $d_{i}(x, y, z)$ both has the same structure: point, or $1-3 \mathrm{D}$ skeleton, and (c). $d_{i}(x, y, z) \leq 0.5$ is included within $f_{a i}(x, y, z) \leq 0.5$.

Step 2: For making the added-material blending region $\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z) \leq 0.5\right.$ and $\left.f_{i}(x, y, z) \geq 0\right\}$ of $f_{i}=0.5$ become $\left\{(x, y, z) \in R^{3} \mid d_{i}(x, y, z) \geq 0.5\right.$ and $\left.f_{a i}(x, y, z) \leq 0.5\right\}$, vary the outer radius parameter $w_{1}$ of $f_{i}$ by replacing $f_{i}$ with $\left(P \circ T_{a^{*}} \circ\right.$ $\left.d_{i}\right)(x, y, z)$ written by

$$
\begin{equation*}
f_{i}=\left(P \circ T_{a^{*}} \circ d_{i}\right)(x, y, z), i=1, \ldots, \text { or } k, \tag{11}
\end{equation*}
$$

where $T_{a *}(d)$ is $T_{*}(d)$ in Eq. (9) with $w_{1}=d_{i}(x, y, z) / f_{a i}(x, y, z)-1$,
( $P \circ T_{a^{*}} \circ d_{i}$ )'s new blending region is derived by substituting $d_{i}(x, y, z) / f_{a i}(x, y, z)-1$ for $w_{1}$ in $\left\{(x, y, z) \in R^{3} \mid d_{i}(x, y, z) \geq\right.$ 0.5 and $\left.d_{i}(x, y, z) \leq 0.5\left(1+w_{1}\right)\right\}$ yields $\left\{(x, y, z) \in R \mid d_{i}(x, y, z) \geq 0.5\right.$ and $\left.d_{i}(x, y, z) \leq 0.5\left(d_{i}(x, y, z) / f_{a i}(x, y, z)-1+1\right)\right\} \equiv\left\{(x, y, z) \in R^{3} \mid d_{i}(x, y\right.$, $z) \geq 0.5$ and $\left.f_{a i}(x, y, z) \leq 0,5\right\}$, completing the proof. Prove it from influential radii $I_{d}$ and $I_{f a}$ of $d_{i}(x, y, z)$ and $f_{a i}(x, y, z)$. Let $d_{i}(x, y, z)$ be represented by $r / I_{d}$ and $f_{a i}(x, y, z)$ by $r / I_{f a}$. Then for
any point $(x, y, z)$ its influential radius is $0.5\left(1+w_{1}\right) I_{d}=$ $0.5\left(1+r / I_{d} / r / I_{f a}-1\right) I_{d}=0.5\left(1+I_{f a} / I_{d}-1\right) I_{d}=0.5 I_{f a}$, bounded by $f_{a i}(x$, $y, z)=0.5$ and so completing the proof.

### 4.2. Field functions with surface-defined inner radius for an intersection blend $B_{l k}\left(f_{1}, \ldots, f_{k}\right)=0.5$

For each primitive in $B_{I k}$, define a field function as described below:
Step 1: Choose a surface $f_{s i}(x, y, z)=0.5$ that satisfy the conditions: (a). $f_{s i}(x, y, z)$ is ray-linear, (b). it and $d_{i}(x, y, z)$ both have the same structure, and (c). surface $f_{s i}(x, y, z) \leq 0.5$ is included within $d_{i}(x, y, z) \leq 0.5$.

Step 2: For making the subtracted-material blending region $\left\{(x, y, z) \in R^{3} \mid f_{i}(x, y, z) \geq 0.5\right.$ and $\left.f_{i}(x, y, z) \geq 1\right\}$ of $f_{i}=0.5$ become $\left\{(x, y, z) \in R^{3} \mid d_{i}(x, y, z) \leq 0.5\right.$ and $\left.f_{s i}(x, y, z) \geq 0.5\right\}$, vary the outer radius parameter $w_{2}$ of $T * \operatorname{in} f_{i}$ by replacing $f_{i}$ with $\left(P \circ T_{s^{*}} \circ\right.$ $\left.d_{i}\right)(x, y, z)$ written by

$$
\begin{equation*}
f_{i}=\left(P \circ T_{s^{*}} \circ d_{i}\right)(x, y, z), i=1, \ldots, \text { or } k, \tag{12}
\end{equation*}
$$

where $T_{s^{*}}(d)=T *(d)$ where $w_{2}=1-d_{i}(x, y, z) / f_{s i}(x, y, z)$,
( $P \circ T_{s^{*}} \circ d_{i}$ )'s new blending region is derived by substituting 1- $d_{i}(x, y, z) / f_{s i}(x, y, z)$ for $w_{2}$ in $\left\{(x, y, z) \in R^{3} \mid d_{i}(x, y, z) \leq 0.5\right.$ and $\left.d_{i}(x, y, z) \geq 0.5\left(1-w_{2}\right)\right\}$ yields $\left\{(x, y, z) \in R \mid d_{i}(x, y, z) \leq 0.5\right.$ and $\left.d_{i}(x, y, z) \geq 0.5\left(1-\left(1-d_{i}(x, y, z) / f_{s i}(x, y, z)\right)\right)\right\} \equiv\left\{(x, y, z) \in R^{3} \mid d_{i}(x, y, z) \geq\right.$ 0.5 and $\left.f_{s i}(x, y, z) \geq 0,5\right\}$, completing the proof. Prove it from influential radii $I_{d}$ and $I_{f s}$ the same as in Eq. (11). Then for any point $(x, y, z)$ its influential radius is $0.5\left(1-w_{2}\right) I_{d}=0.5(1-(1-$ $\left.\left.r / I_{d} / r / I_{f s}\right)\right) I_{d}=0.5\left(I_{f s} / I_{d}\right) I_{d}=0.5 I_{f s}$, bounded by $f_{s i}(x, y, z)=0.5$ and so completing the proof.

For example, Figure 6(a) display a soft object of a elliptic cylinder $\left(P_{b} \circ d_{i}\right)=0.5$ and $d_{i}=\left(\left(\left(|x / 10|^{2}+\left(y /\left.6\right|^{2}\right)^{1 / 2}\right)^{10}+\mid z / 25\right.\right.$ $\left.\left.\right|^{10}\right)^{1 / 10}$, whose level surfaces $\left(P_{b} \circ d_{i}\right)=l, l=0.5,0.35,0.15$, 0.01 , are always similar as in Figure 6(b). However, if the soft object is defined by $\left(P_{b} \circ T_{a n} \circ d_{i}\right)=0.5$ in Eq. (11) possessing $f_{a i}(x, y, z)=\left(|x / 24|^{10}+\left(y /\left.15\right|^{10}+|z / 50|^{10}\right)^{1 / 10}\right.$ shown in Figure 6(a) instead, then level surfaces $\left(P_{b} \circ T_{a n} \circ d_{i}\right)=l, l=0.5$ $0.35,0.15,0.01$, enlarge from $d_{i}(x, y, z)=0.5$ to $f_{a i}(x, y, z)=0.5$ as in Figure 6(d); if the soft object is defined by $\left(P_{b} \circ T_{s^{*}} \circ\right.$ $\left.d_{i}\right)=0.5$ in Eq. (12) with $f_{s i}(x, y, z)=\left(\left(\left(|x / 4|^{2}+\left(y /\left.4\right|^{2}\right)^{1 / 2}\right)^{10}+\mid z /\right.\right.$ $\left.\left.12.5\right|^{10}\right)^{1 / 10}$ shown in Figure 6(e) instead, then level surfaces $\left(P_{b} \circ T_{s^{*}} \circ d_{i}\right)=l, l=0.5,0.65,0.85,0.99$, shrink from $d_{i}(x, y, z)$ $=0.5$ to $f_{s i}(x, y, z)=0.5$ as in Figure 6(f).

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(a)

(b)

(c)


(e)

(f)


Figure 6. (a). soft object of an elliptic cylinder $\left(P_{b} \circ d_{i}\right)=0.5$. (b). Level surfaces $\left(P_{b} \circ d_{i}\right)=l, l=0.5,0.35,0.15,0.01$. (c). Modulation surface $f_{a i}(x, y, z)=0.5$ for $\left(P_{b} \circ T_{a n} \circ d_{i}\right)=0.5$ in (e). (d). Level surfaces $\left(P_{b} \circ T_{a n} \circ d_{i}\right)=l, l=0.5,0.35,0.15,0.01$. (e). Modulation surface $f_{s i}(x, y, z)=0.5$ for $\left(P_{b} \circ T_{s n} \circ d_{i}\right)=0.5$ in (f). (f). Level surfaces $\left(P_{b} \circ T_{s n} \circ d_{i}\right)=l, l=0.5,0.65,0.85,0.99$.

### 4.3. Field functions with a surface-defined inner and an outer radius for a difference blend $B_{D k}\left(f_{1}, f_{2}, \ldots, f_{k}\right)=0.5$

In a difference blend $B_{D k}\left(f_{1}, f_{2}, \ldots, f_{k}\right)=0.5$, the transition is generated in the outer radii of primitives except $f_{1}$, so

- For subtracted primitive $f_{1}$ in $B_{D k}$, define a field function as stated in Eq. (12) such that $\boldsymbol{f}_{\mathbf{1}}=\left(P \circ T_{s^{*}} \circ d_{1}\right)(x, y, z)$ has a new subtracted-material blending region:

$$
\left\{(x, y, z) \in R^{3} \mid d_{1}(x, y, z) \leq 0.5 \text { and } f_{s 1}(x, y, z) \geq 0,5\right\} .
$$

- For each of subtracting primitives $f_{i}, i=2, \ldots, k$ in $B_{D k}$, define a field function as described in Eq. (11) such that $f_{i=}\left(P \circ T_{a^{*}} \circ d_{i}\right)(x, y, z)$ has a new added-material blending region

$$
\left\{(x, y, z) \in R^{3} \mid d_{i}(x, y, z) \geq 0.5 \text { and } f_{a i}(x, y, z) \leq 0.5\right\} .
$$

### 4.4. Transformation function $T *(d)$ for ( $P$ 。

$\left.T_{a^{*}} \circ d_{i}\right)(x, y, z)$ and $\left(P \circ T_{s^{*}} \circ d_{i}\right)(x, y, z)$

This section presents some transforms that are suitable for being used as $T *(d)$ in Eqs. (11)-(12).
4.4.1. Transformation function $T_{*}(d)$ for obtaining a sur-face-defined outer radius in Eq. (11)

- Modulation by $T_{n}(d)$ in Eq. (10).
$T_{n}(d)$ satisfies the mapping requirement $\left[0.5,0.5\left(1+w_{1}\right)\right]$ to $[0.5,1]$, but it need to make sure that $w_{2} \leq 2 w_{1}$ and $w_{2} \leq 1$ hold while varying $w_{1}$. Hence, when applied in Eq. (11) $w_{1}$ and $w_{2}$ of $T_{n}(d)$ need to be modified additionally as follows:

$$
w_{1} \text { of } T_{n}(d)=d_{i}(x, y, z) / f_{a i}(x, y, z)-1 \text { and }
$$

$w_{2}$ of $T_{n}(d)=1$ for $w_{1}>0.5$ or $w_{2}$ of $T_{n}(d)=2 w_{1}$ for $w_{1} \leq 0.5$.
Varying $w_{2}$ by $w_{1}$ such that $w_{2} \leq 2 w_{1}$ is important for performing bulge elimination because $w_{1}$ approaches to zero very often.

- Modulation by $\log$ function $T_{l}(d)$ :
$T_{l}(d)$ defined below maps $\left[0,0.5\left(1+w_{1}\right)\right]$ to $[0,1]$ and 0.5 to 0.5 :

$$
T_{l}(d)=\left\{\begin{array}{cl}
1 & d>0.5\left(1+w_{1}\right)  \tag{13}\\
(2 m d)^{\log (0.5) / \log (m)} & d \leq 0.5\left(1+w_{1}\right)
\end{array}\right.
$$

where $\ln (t)$ denotes $\log (t)$ function and $m=1 /\left(1+w_{1}\right)$ and $w_{1}>0$. $T_{l}(d)$ can be applied in Eq. (11) to adjust the outer radius by varying $w_{1}$.

Soft objects $\left(P \circ T_{a n} \circ d_{i}\right)(x, y, z)=0.5$ and $\left(P \circ T_{a l} \circ\right.$ $\left.d_{i}\right)(x, y, z)=0.5$ offer an added-material blending region: $\left\{(x, y, z) \in R \mid d_{i}(x, y, z) \geq 0.5\right.$ and $\left.f_{a i}(x, y, z) \leq 0.5\right\}$, and the latter one do not need to vary $w_{2}$ by $w_{1}$.
4.4.2 Transformation function $T_{*}(d)$ for obtaining a sur-face-defined inner radius in Eq. (12)

- $T_{n}(d)$ in Eq. (10).
$T_{n}(d)$ also satisfies the mapping requirement $\left[0.5\left(1-w_{2}\right)\right.$, 0.5 ] to [ $0,0.5$ ]. Hence, when applied in Eq. (12), to satisfy $w_{2} \leq 2 w_{1} w_{1}$, and $w_{2}$ of $T_{n}(d)$ can be set additionally by:

$$
w_{2}=1-d_{i}(x, y, z) / f_{s i}(x, y, z) \text { and } w_{1}=w_{2} .
$$

## - Modulation by $\log$ function $T_{r}(d)$ :

Transform $T_{r}(d)$, defined below, maps $\left[0.5\left(1-w_{2}\right), 1\right]$ to $[0$, $1]$ and 0.5 to 0.5 .

$$
T_{r}(d)=\left\{\begin{array}{cl}
0 & d<0.5\left(1-w_{2}\right)  \tag{14}\\
1-(2 m(1-d))^{\log (0.5) / \log (m)} & d \geq 0.5\left(1-w_{2}\right)
\end{array}\right.
$$

where $m=1 /\left(1+w_{2}\right)$ and $0<w_{2} \leq 1 . T_{r}(d)$ can be applied in Eq. (12) to adjust the inner radius by varying $w_{2}$.

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Soft objects $\left(P \circ T_{s n} \circ d_{i}\right)(x, y, z)=0.5$ and $\left(P \circ T_{s r} \circ d_{i}\right)(x, y, z)$ $=0.5$ offer a subtracted-material blending region $\{(x, y, z) \in R \mid$ $f_{s i}(x, y, z) \geq 0,5$ and $\left.d_{i}(x, y, z) \leq 0.5\right\}$ without varying $w_{1}$.

### 4.5. Ray-linear $f_{a i}(x, y, z)$ and $f_{s i}(x, y, z)$

Because $f_{a i}(x, y, z)$ and $f_{s i}(x, y, z$ in Eqs. (11)-(12) need to be ray-linear, this section shows an easy way to create a raylinear function. As stated in [6], if $B_{k}\left(x_{1}, \ldots, x_{k}\right)$ is ray-linear and primitives $f_{1}, \ldots$, and $f_{k}$ are ray-linear, then blend $B_{k}\left(f_{1}, \ldots, f_{k}\right)$ is ray-linear, too. So, one may ray-linear blending operators such as union and intersection with range parameters in $[5,6]$ and super-ellipsoidal union and intersection [4] in Eqs. (7)-(8), and then create a ray-linear $f_{a i}(x, y, z)$ and $f_{s i}(x, y, z)$ by performing applying these operators $B_{k}\left(x_{1}, \ldots, x_{k}\right)$ on the following primitives:

- Primitives of parallel planes, denoted as $f(x, y, z)$, to obtain symmetrical modulation surface $B_{k}\left(f_{p 1}, \ldots, f_{p k}\right)=0.5$.

$$
f_{p}(x, y, z)=|[x, y, z] \bullet \vec{n}| / a .
$$

- Primitives of one-branch plane, denoted as $f_{a}(x, y, z)$, to obtain asymmetrical modulation surface $B_{k}\left(f_{o 1}, \ldots, f_{o k}\right)=0.5$.

$$
f_{o}(x, y, z)=[[x, y, z] \bullet \vec{n}]_{+} / a,
$$

where $\left[{ }^{*}\right]_{+} \equiv \operatorname{Max}(*, 0), \vec{n}$ denotes a normal vector toward the plane and • means dot product.

Based on these above, some modulation surfaces that offer six parameters, $t_{1}, t_{2}, t_{3}, t_{4}, t_{5}, t_{6}$ and $\ldots$ to adjust the lengths of positive and negative $x, y$ and $z$ axes, respectively, are created using super-ellipsoidal intersection blends and presented below:
(1). Super-quadrics [23]:

$$
d(x, y, z)=\left(\left(\left|x / a_{1}\right|^{n 1}+\left|y / a_{2}\right|^{n 1}\right)^{n 2 / n 1}+\left|z / a_{3}\right|^{n 2}\right)^{1 / n 2}
$$

and its modulation surface:

$$
\begin{align*}
& f(x, y, z)=\left(\left(\left[x /\left(t_{1} a_{1}\right)\right]_{+}^{n 1}+\left[-x /\left(t_{2} a_{1}\right)\right]_{+}^{n 1}+\left[y /\left(t_{3} a_{2}\right)\right]_{+}^{n 1}+[-\right.\right. \\
& \left.\left.\left.y /\left(t_{4} a_{2}\right)\right]_{+}^{n 1}\right)^{n 2 / n 1}+\left[z /\left(t_{5} a_{3}\right)\right]_{+}^{n 2}+\left[-z /\left(t_{6} a_{3}\right)\right]_{+}^{n 2}\right)^{1 / n 2} \tag{15}
\end{align*}
$$

(2). Generalized distance function [10]:

$$
d(x, y, z)=\left(\sum_{i=1}^{k}\left(\left|[x, y, z] \cdot \vec{n}_{i} / a_{i}\right|^{n}\right)\right)^{1 / n}
$$

and its modulation surface:
$f(x, y, z)=$

$$
\begin{equation*}
\left(\sum_{i=1}^{k}\left(\left[[x, y, z] \bullet \vec{n}_{i} /\left(t_{i} a_{i}\right)\right]_{+}{ }^{n}+\left[[-x,-y,-z] \bullet \vec{n}_{i} /\left(t_{2 i} a_{i}\right)\right]_{+}^{n}\right)^{1 / n}\right. \tag{16}
\end{equation*}
$$

(3). Spherical cross-product function [14]:

Given two 2D functions $h(x, y)$ and $m(x, z)$ by

$$
h(x, y)=\left(\left|x / a_{1}\right|^{n}+\left|y / a_{2}\right|^{n}\right)^{1 / n} \text { and } m(x, z)=\left(x^{n}+\left|z / a_{3}\right|^{n}\right)^{1 / n},
$$

then a cross-product function $d(x, y, z)$ is written by

$$
d(x, y, z)=m(h(x, y), z),
$$

which can also vary to generate super-elliptic cylinders (Line skeletons):

$$
\begin{equation*}
d(x, y, z)=m\left(h(x, y), \operatorname{Sign}(z)[|z|-L]_{+}\right), \tag{17}
\end{equation*}
$$

where $\operatorname{Sign}(*)$ srands for 1 if $*>0$, otherwise $-1, d(x, y, z)=1$ has a cross-section $h(x, y)=1$ and his spine is along $z$ axis and $2 L$ long.

As for the modulation surfaces for Eq. (17), just replace $h(x, y)$ and $m(x, z)$ with:

$$
\begin{equation*}
h(x, y)=\left(\left(\left[x /\left(t_{1} a_{1}\right)\right]_{+}^{n}+\left[-x /\left(t_{2} a_{1}\right)\right]_{+}^{n}+\left[y /\left(t_{3} a_{2}\right)\right]_{+}^{n}+\left[-y /\left(t_{4} a_{2}\right)\right]_{+}^{n}\right)^{1 / n}\right. \tag{18}
\end{equation*}
$$

and $\quad m(x, z)=\left(x^{n}+\left[z /\left(t_{5} a_{3}\right)\right]_{+}^{n}+\left[-z /\left(t_{6} a_{3}\right)\right]_{+}^{n}\right)^{1 / n}$.

## 5. Applications

Once primitive soft objects are defined using field functions $\left(P \circ T_{s^{*}} \circ d_{i}\right)(x, y, z)$ in Eqs. (11) and (12), soft blend, Ricci's and Perlin's set blends are allowed to have the following applications by choosing suitable modulation surfaces $f_{c i}(x, y, z)=0.5$ as described below:
(1).Application 1: Bulge elimination for a soft blend or a Perlin and Ricci's union blend of interconnecting or intersecting super-elliptic cylinders and super-toroids:
Even though gradient-based methods [12, 15] is not suitable for these blends to eliminate bulges due to lacking range parameters, the bulges cam also be eliminated by defining primitives by $f_{i}=\left(P \circ T_{s^{*}} \circ d_{i}\right)(x, y, z), i=1, . ., k$, and then choosing modulation surfaces $f_{a i}(x, y, z)=0.5$ without containing the regions where unnecessary bulges lie.

As shown in Fig. 7(a), in order to eliminate bulge cylinders 1 and 2 need modulation surfaces $f_{a}(x, y, z)=0.5$ that do not contain the top and the bottom regions above and below the cylinders shown in Fig. 7(b). Fortunately, super-quadrics, generalized distance function, super-elliptic cylinder in Eqs. (15)-(17) offer the ability to generate or avoid a blend on the Right, Left, Top, Bottom, Front or Rear region of them, as displayed respectively in Fig. 7(c), by setting $t_{i}, i=1-6$, instead of $t_{i} a_{*}$, as described below:

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- Setting $t_{i} \geq 2$, for generating a blend;
- Setting $t_{i}=1+\omega / a_{*}$, for bulge eliminations, where $\omega \cong 0$ such as $\omega=0.1 \sim 0.05$ and $*$ is the integer greater than or equal to $i / 2$.


Figure 7. (a). Bulge needed to be removed. (b)-(d). The parameters for adjusting the Right, Left, Top, Bottom, Front and Rear regions of a cylinder that bulges might occur on.

For example, Fig. 8(a) shows three super-elliptic cylinders $d(x, y, z)=0.5, n=2,4$, and 8 :

$$
d(x, y, z)=m\left(h(x, y), \operatorname{Sign}(z)[|z|-16]_{+}\right)
$$

where

$$
\begin{aligned}
& h(x, y)=\left(|x / 6|^{n}+|y / 6|^{n}\right)^{1 / n} \text { and } \\
& m(x, z)=\left(x^{n}+|z / 6|^{n}\right)^{1 / n}
\end{aligned}
$$

Fig. 8(b) shows a chair containing many bulges on the intersecting and connecting regions because it is defined by Perlin union $B_{P U}\left(f_{1}, \ldots, f_{14}\right)$ in Eq. (4) of cylinders $f_{i}=(P$ 。 $\left.d_{i}\right)(x, y, z), i=1$ to 14 where $d_{i}=d(x, y, z)$ and $n=8$. However, if $f_{i}$ is defined by $\left(P \circ T_{a n} \circ d_{i}\right)(x, y, z)$ instead and modulation surface $f_{a i}=0.5, i=1$ to 14 is defined by Eq.(17). Thus, the bulges of Fig. 8(b) are removed as shown in Fig. 8(c) by setting $t_{i}=(1+0.1 / 6)$ to exclude those blending regions where bulges lie; for example, $f_{a}=0.5$ of cylinders 1 and 2 are defined by

$$
f_{a}(x, y, z)=m\left(h(x, y), \operatorname{Sign}(z)[|z|-16]_{+}\right)
$$

where

$$
\begin{aligned}
& h(x, y)=\left(\left([x /(2 * 6)]_{+}^{n}+[-x /(2 * 6)]_{+}^{n}+[y /((1+0.1 / 6) 6)]_{+}^{n}+[-y /((1+\right.\right. \\
& \left.0.1 / 6) 6]]_{+}^{n}\right)^{1 / n} \text { and } \\
& m(x, z)=\left(x^{n}+[z /((1+0.1 / 6) 6)]_{+}{ }^{n}+[-z /((1+0.1 / 6) 6)]_{+}{ }^{n}\right)^{1 / n} .
\end{aligned}
$$

In a union blend $B_{U 3}\left(f_{1}, f_{2}, f_{3}\right)=0.5$, if the blending region of $f_{1}$ overlaps with those of $f_{2}$ and $f_{3}$ at two places, then two blends will be generated. However, $f_{1}$ can avoid the blend with $f_{3}$ but keep the one with $f_{3}$ unchanged, by defining them using $\left(P \circ T_{a m} \circ d_{i}\right)$ and then choosing a modulation surface $f_{a 1}=0.5$ such that $f_{1}$ 's new blend region $\left\{(x, y, z) \in R \mid d_{1}(x, y, z) \geq\right.$ 0.5 and $\left.f_{a 1}(x, y, z) \leq 0.5\right\}$ does not touch $f_{3}$ 's blend region.


Figure 8. (a). Cylinders with contours $\left(x^{n}+y^{n}\right)^{1 / n}=1, i=2,4,8$. (b). Perlin's union of interconnecting cylinders that generates bulges. (c). The bulges in (b) are eliminated by defining cylinders using $\left(P \circ T_{a n} \circ d_{i}\right)$ and $d_{i}$ and $f_{a i}(x, y, z)$ using Eq. (18), and then setting $t_{i}$ by Eq. (19) to eliminate unwanted bulges.

For example, Fig. 9(d) displays a soft blend $B_{S U 3}\left(f_{1}, f_{2}, f_{3}\right)$ $=0.5$ of $f_{i}=\left(P_{b} \circ T_{a n} \circ d_{i}\right)(x, y, z)=0.5, i=1,2,3$, where cylinder $f_{1}=0.5$ generates two blends respectively with cylinder $f_{2}=0.5$ and toroid $f_{3}=0.5$. However, one can choose a new $f_{a \underline{1}}=0.5$ for $f_{1}=0.5$ such that the new region $f_{a 1}(x, y, z) \leq 0.5$ in Fig. 9(e) is shorter than the original one in Fig 9 (f) and so the unwanted blend in region $b$ is removed but the one in region $a$ is still kept unchanged as in Fig. 9(g). The new and old $f_{a 1}(x, y, z)$ and $d_{1}(x, y, z)$ are written below:

$$
\begin{aligned}
& \text { new } f_{a 1}(x, y, z)=\text { old } f_{a 1}(x, y, z)= \\
& d_{1}(x, y, z)=m\left(h(x, y), \operatorname{Sign}(z)[|z|-16]_{+}\right)
\end{aligned}
$$

where new $f_{a 1}(x, y, z)$, old $f_{a 1}(x, y, z)$ and $d_{1}(x, y, z)$ they have different definitions of $h(x, y)$ and $m(x, z)$, respectively, by
(a). $h(x, y)=\left(|x / 6|^{n}+|y / 6|^{n}\right)^{1 / n}$ and $m(x, z)=\left(x^{n}+|z / 6|^{n}\right)^{1 / n}$ for $d_{1}$,
(b). $h(x, y)=\left(\left([x /(2 * 6)]_{+}{ }^{n}+[-x /(2 * 6)]_{+}{ }^{n}+[y /((1+0.1 / 6) 6)]_{+}{ }^{n}+[-\right.\right.$ $\left.y /((1+0.1 / 6) * 6)]_{+}{ }^{n}\right)^{1 / n}, \quad$ and $\quad m(x, z)=\left(x^{n}+[z /(2 * 6)]_{+}{ }^{n}+\left[-z /\left(2^{*}\right.\right.\right.$ $\left.6)]_{+}{ }^{n}\right)^{1 / n}$ for old $f_{a 1}$, and

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(c). $h(x, y)=\left(\left([x /(2 * 6)]_{+}{ }^{n}+[-x /(2 * 6)]_{+}+[y /((1+0.1 / 6) 6)]_{+}{ }^{n}+[-y /\right.\right.$ $\left.\left.\left((1+0.1 / 6)^{*} 6\right)\right]_{+}{ }^{n}\right)^{1 / n}, \quad m(x, z)=\left(x^{n}+[z /((1+0.2 / 6) 6)]_{+}{ }^{n}+[-z /((1+\right.$ $\left.0.2 / 6) 6)]_{+}{ }^{n}\right)^{1 / n}$ for new $f_{a 1}$.

(d)

(e)

(f)

(g)


Figure 9. (a). Cylinder $f_{1}=0.5$. (b). Cylinder $f_{2}=0.5$. (c). Toroid $f_{3}=0.5$. (d). Soft blend of soft objects $f_{1}, f_{2}$ and defined using $f_{i}=\left(P_{b} \circ T_{s m} \circ d_{i}\right), i=1,2,3$, on which two blends are generated at regions $a$ and $b$. (e). New $f_{a 1}=0.5$ for $f_{1}$. (f). Original $f_{a 1}=0.5$ for $f_{1}$. (g). Because new $f_{a 1}=0.5$ in (e) is shorter than the one in ( $f$ ), the unwanted blend at region $b$ is removed.

## 6. Conclusion

Compared to other existing blends, although soft blend, Ricci's and Perlin's set blends have lower computing complexity, they can do nothing or little for shape control, bulge elimination and avoiding unwanted blends because of lacking range parameters and the similarity of the level surfaces of existing field functions. However, if primitive soft object are defined by using the proposed field functions with sur-face-defined influential radii as defining functions. Because the proposed filed functions allow freely choosing modulation surfaces to change primitives' added-material and sub-tracted-material blend regions, soft blend, Ricci's and Perlin's set blends not only have lower computing complexity than other blends but also have the following additional applications:
(1). They can perform bulge elimination on intersecting su-per-elliptic cylinders and toroids although they do not have range parameters for bulge elimination using gradient-based methods.
(2). They can do bulge elimination on high-dimensional blends.
(3). They can remove unwanted blends.

## Appendix

A. Definition 1: A function $f(x, y, z): R^{3} \rightarrow R_{+}$is called nonnegative ray-linear if $f(a(x, y, z))=a f(x, y, z)$ holds for any $(x, y, z) \in R^{3}$ and $a \in R_{+}$.
B. Theorem 1: If $f(x, y, z): R^{3} \rightarrow R_{+}$is non-negative ray-linear, then $f(x, y, z)$ can be reformulated as $r / I_{f}$, where $r=\left(x^{2}+y^{2}+z^{2}\right)^{0.5}$ and $I_{f}$ is the distance from the origin to the intersecting point of the vector $[x, y, z]$ with the surface $f(x, y, z)=1$.

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## Biographies

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